

P.N.Lebedev Physical Institute
of Russian Academy of Sciences

National Research
Nuclear University «MEPhI»

**CONCEPTION of CRYOGENIC TARGET FACTORY
for MASS MANUFACTURING & HIGH-REP-RATE
DELIVERY of the IFE TARGETS**

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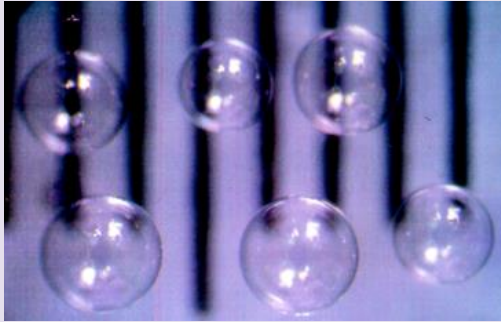
Academic Programs and External Partners

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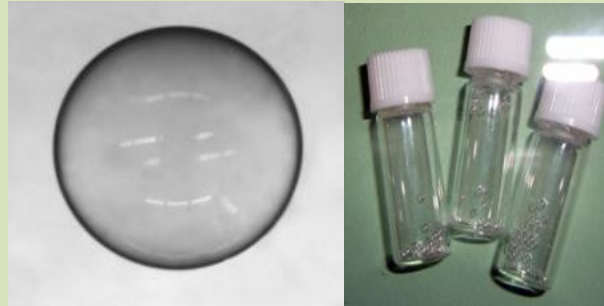
Polymer (CH) shells used in our researches

Russia



CH shells of \varnothing 1,0—1,8 mm made at LPI, Russia

UK



CH shell of $\sim \varnothing$ 2 mm and a shell batch made at STFC, UK

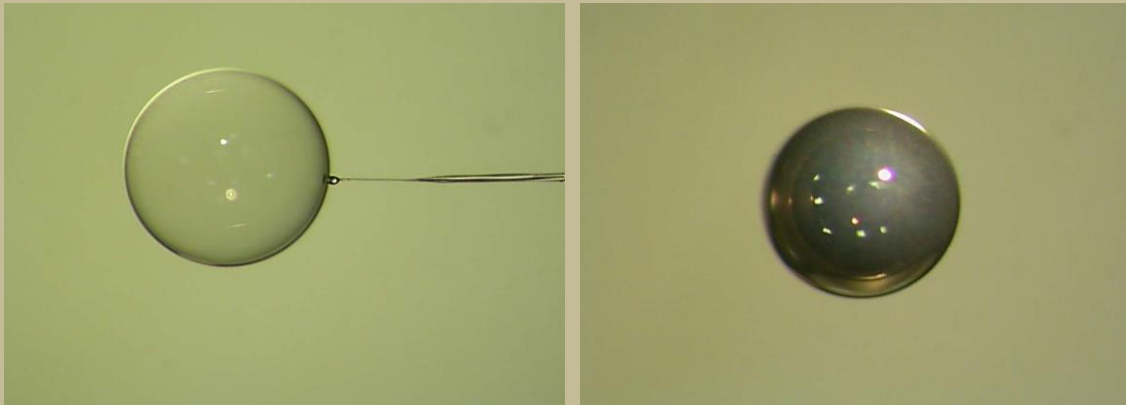
CH shell is an important element of the cryogenic target

■ In our research we have used CH shells ($\varnothing \leq 1.8$ mm) made at the Termonuclear Target Lab. of the Lebedev Physical Institute (LPI, Russia)

■ Large CH shells ($\varnothing \geq 1.8$ mm) have been delivered by the Science & Technology Facility Council (STFC, UK)

■ CH shells covered with a thin layer of Pb have been delivered by the Institute for Laser Engineering (ILE, Osaka Univ., Japan).

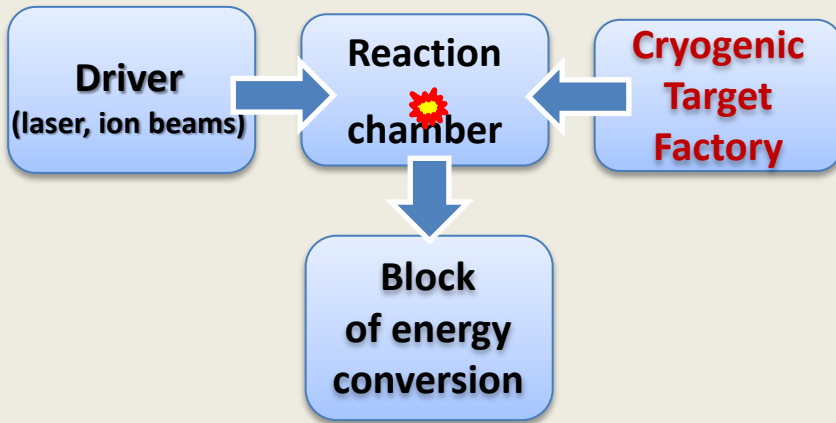
Japan



Pb coated CH shell of $\sim \varnothing$ 2 mm (at T=5K) made at ILE, Japan

Cryogenic Target Factory (CTF) is a main building block of IFE reactor

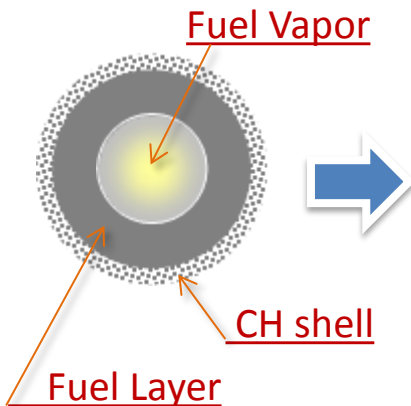
Main building blocks of IFE reactor



CTF main specifications

1. Free-standing targets mass-production: ~ 1 000 000 targets/day (upon the average)
2. High rep-rate target delivery:
 - injection velocity of 200 - 400 m/s
 - rep-rate of ~10 Hz (laser) or 0.1 Hz (Z-pinch)
3. Survivability of a fuel core during target delivery
4. On-line characterization of a flying target
5. Tritium inventory minimization

Direct-drive Cryogenic Fuel Target



Fuel layer specifications

- Thickness non-uniformity: $Nu < 1.0\%$
- Inner surface roughness: $\delta < 1 \text{ um}$ rms in all modes

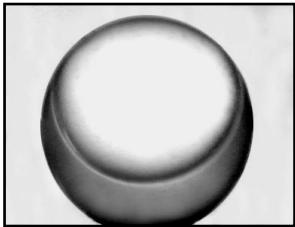
CTF critical issue:

Development of the RELIABLE, EFFECTIVE, and INEXPENSIVE METHODS of CRYOGENIC TARGETS MASS - PRODUCTION

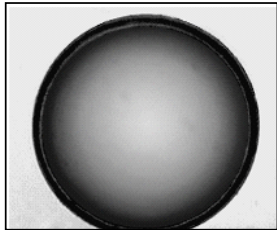
LPI CONTRIBUTION TO THE PROBLEM OF CRYOGENIC TARGETS MASS-PRODUCTION

⇒ FST LAYERING METHOD ⇒ Fuel layering in the moving free-standing targets ⇒ FST layering goes during $t < 15$ s. Free-standing targets move one-by-one in the LM.

Initial cryogenic target with liquid D_2 -fuel



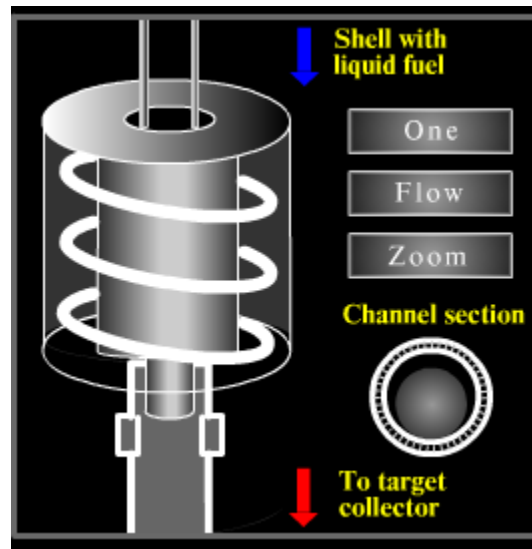
Finished cryogenic target with solid D_2 layer



CH shell: \varnothing 1.23 mm
Layer: 41 μ m, $D_2+20\%$ Ne
 $Nu < 2\%$, $\delta < 0.5$ μ m

FST Layering during $t < 15$ sec

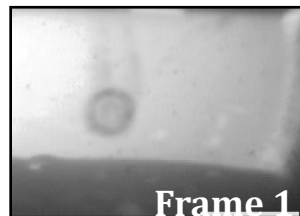
FST-layering module (LM):
general view & physical layout



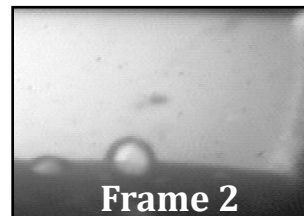
Cryogenic experiment with FST-layering module



Cryogenic target injection into the test chamber at 5 K

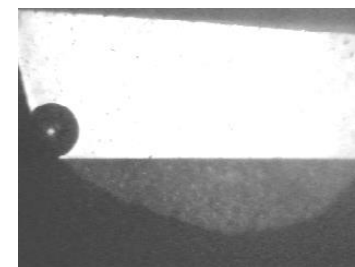


Target in free-fall

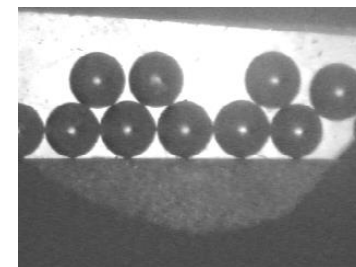


Target landing

Rep-rated injection of 1 mm targets at 5K, $f = 0.1$ Hz (batch mode)



$t = 0$



$t = 100$ s

Our calculations have shown that isotropic ULTRAFINE FUEL LAYER is required for target survival in the delivery process

SOLID H₂ ISOTOPES IN EQUILIBRIUM: ANISOTROPIC MOLECULAR HCP - CRYSTALS

◆ **HEXAGONAL CRYSTALS** ⇒ sound velocity v depends on sound wave line about the crystallographic axes. The difference in sound velocity for H₂-crystal reach **33%** [Phys.Lett. 1972]

◆ **MOLECULAR CRYSTALS** ⇒ mechanism of heat conduction is mainly connected with lattice conductivity, which depends on sound velocity v (Debye`s theory): $k \sim (1/3) c v \Lambda$

MODELING RESULTS

Due to the thermal radiation of the reaction chamber walls, the inner surface of anisotropic fuel layer becomes non-isothermal and degrades before the target arrive at the laser focus (**16 ms**) [J.Phys.D:Appl.Phys. 34, 2004]

To suppress the process of fuel surface degradation we propose to apply isotropic ultrafine fuel layers, which can be created using the FST layering method

DATA FOR CALCULATION: SOMBRERO reaction chamber: radius is 6.5 m, $T_{cr} = 1758$ K, $j = 56$ Wt/cm²; injection velocity of a target: $v_{inj} = 400$ m/sec; time of target flight inside a chamber **16** msec; target T just before irradiation $T=18.5$ K; Target : CH shell of $\varnothing 4$ mm and 45 μ m-thick, fuel D₂-layer of 200 μ m-thick

The FST technology is unique and there is not alternative of that kind

- **FST principle:**
 - Targets are moving and free-standing
 - Target injection between the basic units of the LM
 - Time & space minimization for all production steps, which ensures tritium inventory minimization
- **FST result:**

A batch mode is applied, and high cooling rates are maintained (1-50 K/s) to form **spherically symmetric & smooth isotropic ultra-fine solid layers** inside free-rolling targets
- **FST status:**

FST technology and facilities created on its base are protected by the RF Patent and 3 Invention Certificates



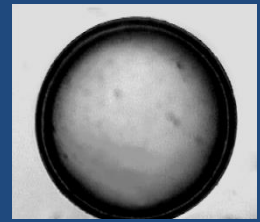
NEXT STEP: FST technology demonstration for cryogenic targets of a reactor scale with rep-rate production up to ~1 Hz and more

Reactor-scale targets: CH shells \varnothing 2-4 mm, layer thickness ~200-300 μ m

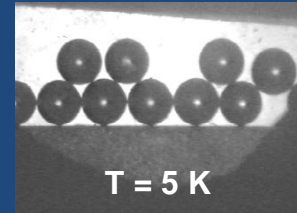
CTF-LPI \Rightarrow The conception of a Cryogenic Target Factory is based on 3 approaches proposed & examined at LPI

- ❑ **FST technology** \Rightarrow mass-production of moving free-standing targets (FST) with ultrafine fuel layer
- ❑ **Injection transport of a target between the CTF subsystems** \Rightarrow gravitational, electromagnetic & magnetic levitation (maglev)
- ❑ **Application of the HTSC quantum levitation effect** for almost frictionless motion of the cryogenic targets at their handling & delivery
- ❑ **Fourier holography** \Rightarrow for flying target tracking

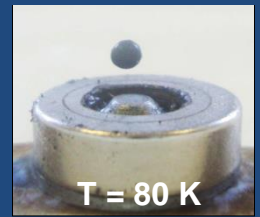
The POP and computer experiments have proved the interaction efficiency of the proposed approaches



FST -layering : free-standing cryo target



Targets injection with the rate of 0.1Hz (batch mode)



HTSC coated CH shell levitating above magnet

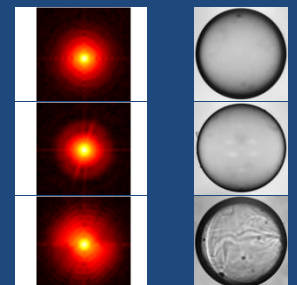
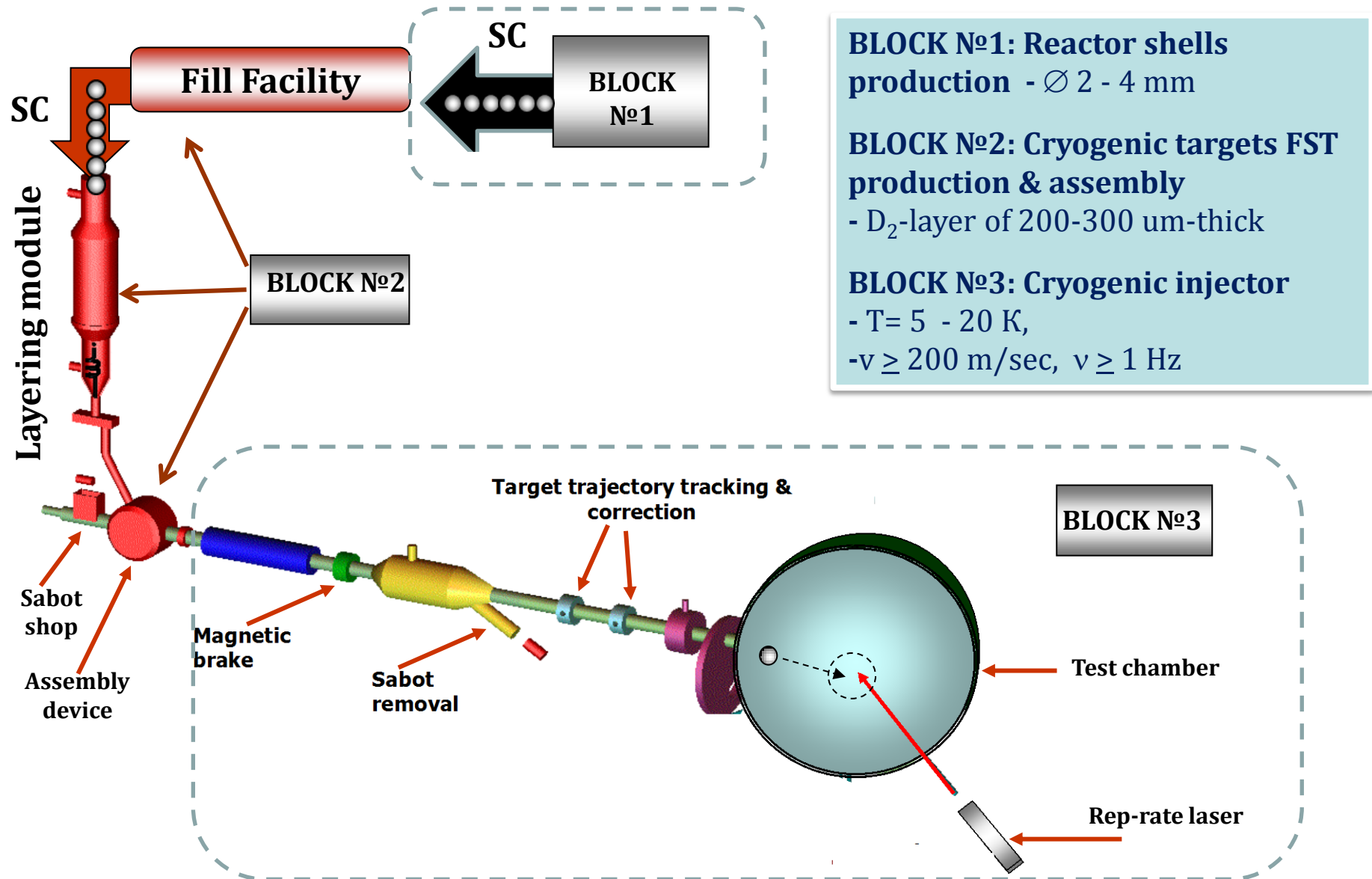


Image Fourier transforms of the shells with different imperfections

CTF-LPI \Rightarrow modular setup for development & fine-tuning of the FST transmission line at a high rep-rate (1-10 Hz)



BLOCK №1: Reactor shells production - \varnothing 2 - 4 mm

BLOCK №2: Cryogenic targets FST production & assembly
- D_2 -layer of 200-300 μ m-thick

BLOCK №3: Cryogenic injector
- $T = 5 - 20$ K,
- $v \geq 200$ m/sec, $\nu \geq 1$ Hz

Basic elements of the **CTF-LPI** have been tested by LPI on the prototypical models. That allows risk minimization at the CTF construction & start-up



Layering module (LM):
FST method for fuel layering
inside free-rolling targets



LPI- & "Red Star" teamwork

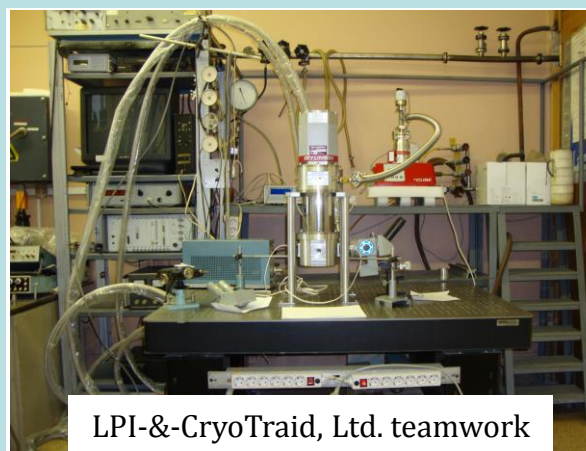
**Startup of the FST facility
at the LPI in 1999**



Fill facility:
Filling of CH shells with gaseous
fuel up to 1000 atm at 300K

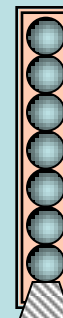


Cryogenic target characterization:
100-projections visual-light tomograph
with 1 um space-resolution



LPI- & CryoTraid, Ltd. teamwork

Transport systems:
Facility for research in the area of HTSC
levitation



Handheld Shell Container (SC)
for fuel filled shells transport at
300 K from the fill system to the
FST-layering module

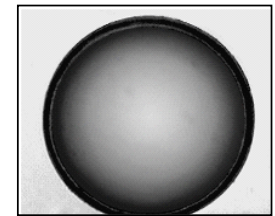
FST facility created at LPI: CURRENT PARAMETERS

⇒ Diffusion ramp filling of a batch of free-standing CH shells up to 1000 atm at 300 K with H_2 , D_2 , or their mixtures (molecular & atomic diffusion mode are available)

⇒ Formation of cryogenic layers inside moving free-standing CH shells \varnothing 0.8–1.8 mm

⇒ Formation of isotropic ultra-fine cryogenic layers. Application of such layer gives the following advantages:

- Delivery process: Enhance mechanical strength & thermal stability of a fuel layer
- Implosion process: Avoid instabilities caused by grain-affected shock velocity variations



CH shell: \varnothing 1.23 mm
Layer: 41 μ m, $D_2+20\%$ Ne
Nu < 2%, δ < 0.5 μ m

⇒ Tritium inventory minimization:

- Fuel filling: minimal spatial scale due to close packing of free-standing targets
- Fuel layering: minimal layering time $t_f < 15$ sec (conventional methods: $t_f \sim 24$ hrs)
- Target transport: minimal transport time between the basic units of the CTF due to realization of injection transport process

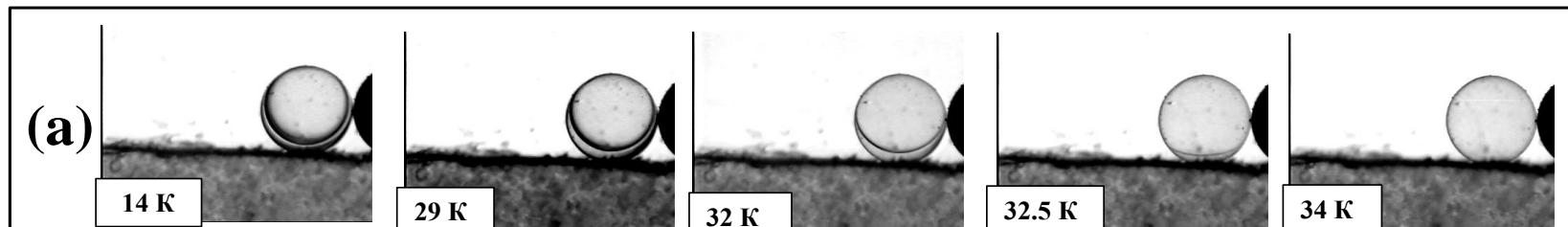
⇒ Rep-rate mode: current production rate is about $\nu = 0.1$ Hz

⇒ FST layering is the most inexpensive technology (< 30 cents per 1 target)

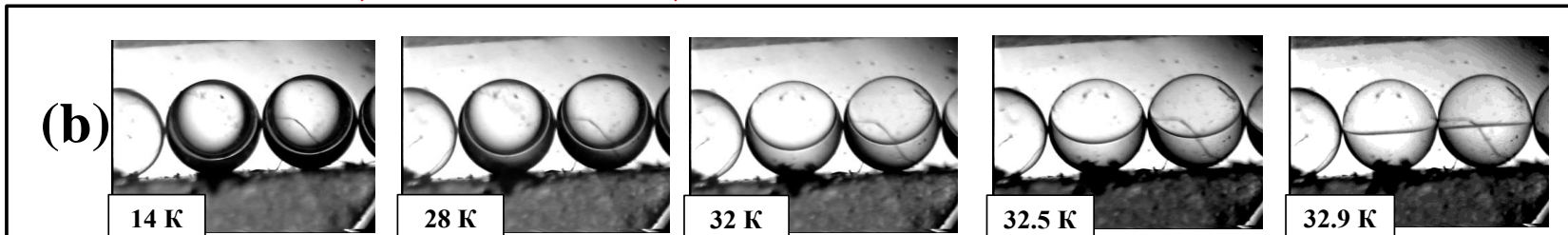
Demonstration of the fill facility operation for CH shells of ~ 1 mm diam.

Vapor bubble behavior inside the cryogenic target as function of temperature and fill pressure P_{fill} (fill density ρ_{fill}) of a fuel

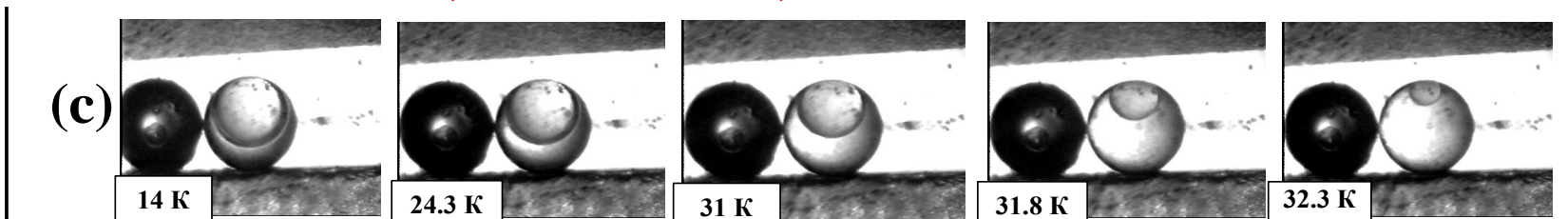
$\frac{V_{vapor}}{V_0} = \alpha^3$	$\alpha(\rho_{fill}, T) = \frac{(\rho_{liquid} - \theta\rho_{cp})^{1/3}}{(\rho_{liquid} - \rho_{vapor})^{1/3}}$	$\theta = \frac{\rho_{fill}}{\rho_{cp}}$
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CH shell \varnothing 940 μ m, $P_{fill} = 305$ atm H_2 , $\theta = 0.69$



CH shell \varnothing 949-953 μ m, $P_{fill} = 445$ atm H_2 , $\theta = 0.93$



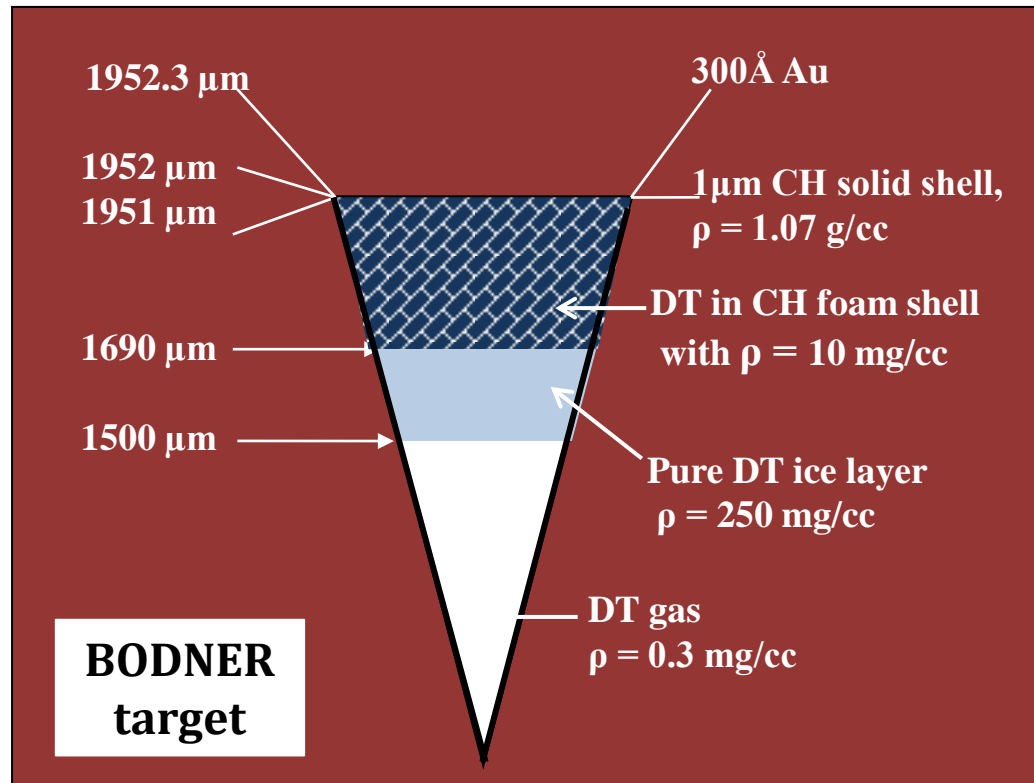
CH shell \varnothing 980 μ m, $P_{fill} = 765$ atm H_2 , $\theta = 1.32$

RESULTS OF CALCULATION: Diffusion fuel filling of a reactor-scaled target

CALCULATED TIME FOR the BODNER TARGET RAMP FILLING

up to a FILL PRESSURE of 1100 atm

Fuel	molecular mode	atomic mode	Notations: t_{md} – time of fuel filling in molecular diffusion mode t_{ad} – time of fuel filling in atomic diffusion mode Shell material - polyimide, $E = 15 \text{ GPa}$; $P_{buckle} = 0.3376 \text{ atm}$
D_2 fuel	$t_{md} = 7 \text{ hrs}$	$t_{ad} \simeq 5 \text{ hrs}$	
DT fuel	$t_{md} \simeq 8 \text{ hrs}$	under consideration	

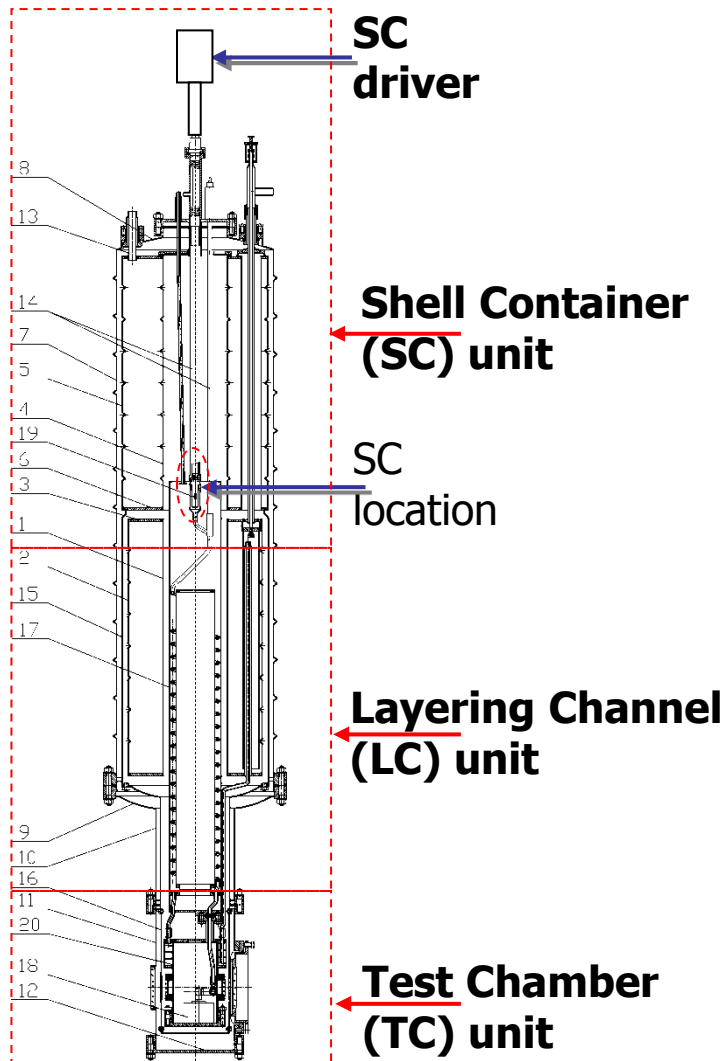


Baseline design of high gain direct-drive target

[Bodner et al. Phys. Plasmas 7, 2298, 2000]

CTF-LPI ⇒ FST-layering module designed by LPI for EU project HiPER can serve as a prototype for 1 Hz operation in a batch mode

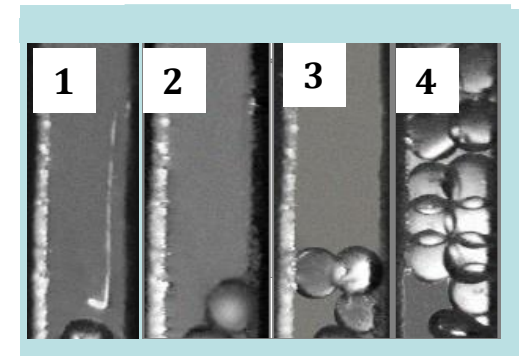
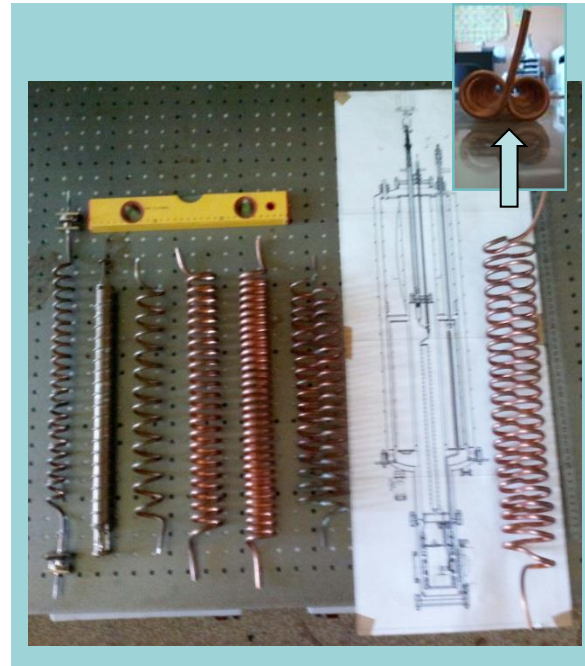
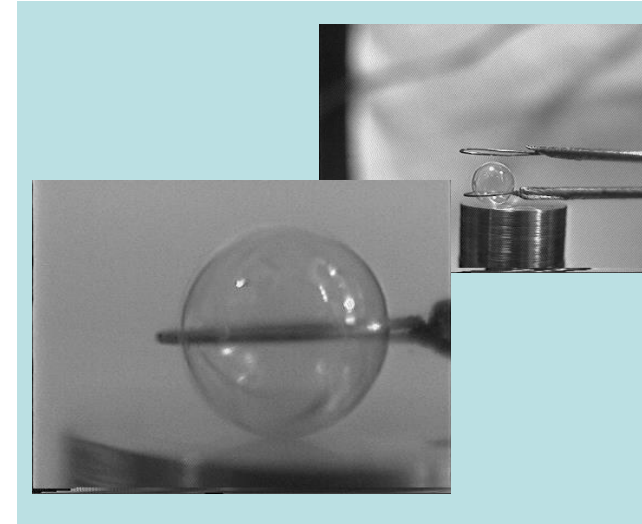
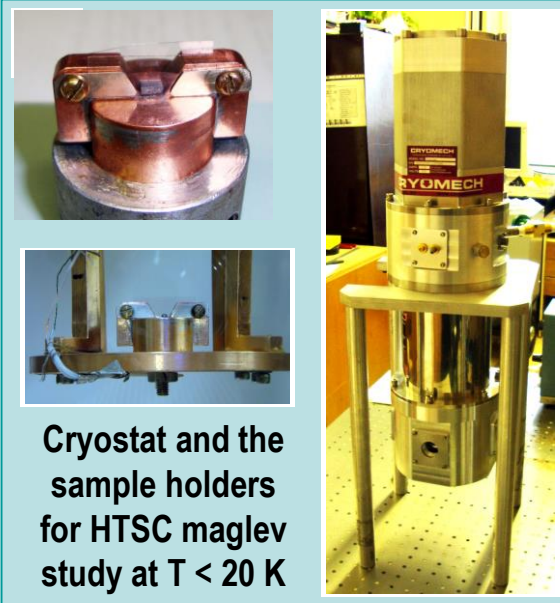
□ Drawing of the FST-layering module



□ General units & estimated weight

FST-layering module	Weight, kg
Helium cryostat (total)	41,3
Helium cryostat casing	16,8
Nitrogen vessel	10,1
Thermal screen	6,9
Outer helium vessel	7,5
Insert (total)	5,88
- sluice-safe unit	2,2
- layering module	2,9
- shaft of lock	0,07
- key	0,71
Optical test chamber (total)	8.95
- helium chamber with PD	2,4
- TC thermal screen	1,0
- TC frame	2,8
- flange	1,45
- windows	0,95
- location bracketry	0,35
Frame (total)	13,7
SC with interface (total)	1,7
SC	0,25
Interface	1,45
TOTAL	71,53

FST-layering module designed for HiPER: we have constructed a number of mockups and carried out the mockups testing to minimize possible risks

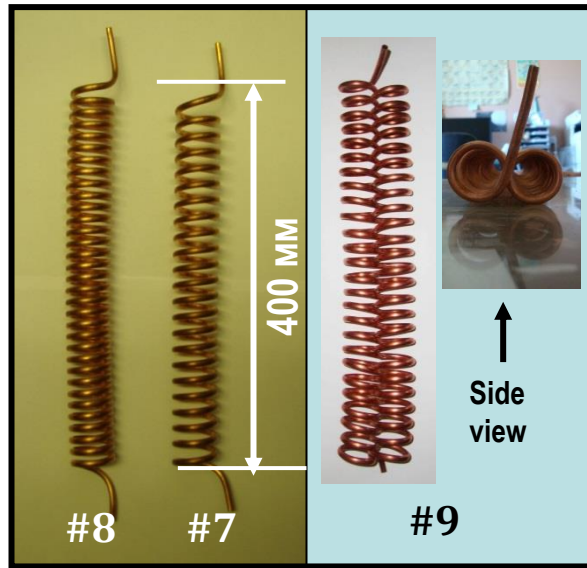


Optical test chamber

A set of the FST-layering channels (LC)

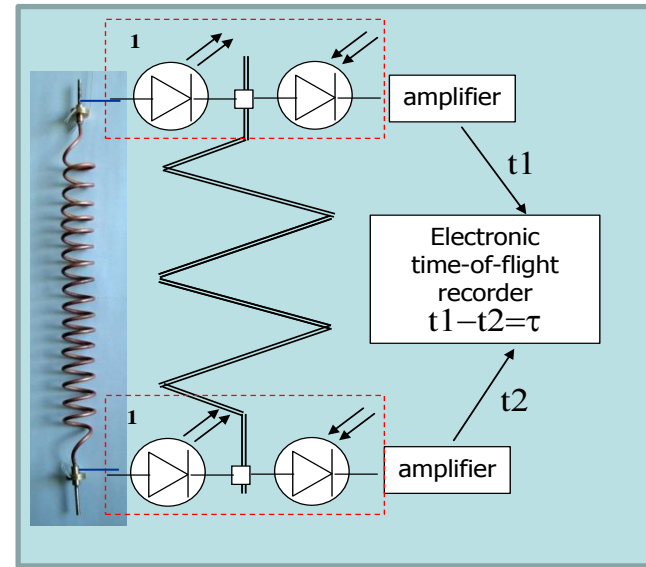
Target collector:
demonstration of targets
gravity injection

EXPERIMENT: a double-spiral FST-layering channel (LC) is a good prospect for reactor targets production



Mockups of the spiral LC

#7, #8 \Rightarrow single-spiral LC (SSLC),
#9 \Rightarrow double-spiral LC (DSL),
Copper tube OD=38mm



Schematics of measuring the time
of target movement inside the LC
1 - optronics couple made from IR-diodes

Calculations

FST-layering time for
reactor-class targets

$$t_l \geq 16 \text{ s}$$

Experiment

t_m - time of target movement in a channel, data averaged for 10 shots

SSLC

$$t_m \leq 16 \text{ s}$$

DSL

$$t_m = 23.5 \text{ s}$$

FOURIER HOLOGRAPHY OF IMAGE RECOGNITION: promising way for on-line characterization of a flying target [Nikitenko, et al. Nuclear Fusion, 2006]

Computer experiments demonstrated much promise of Fourier holography because it allows

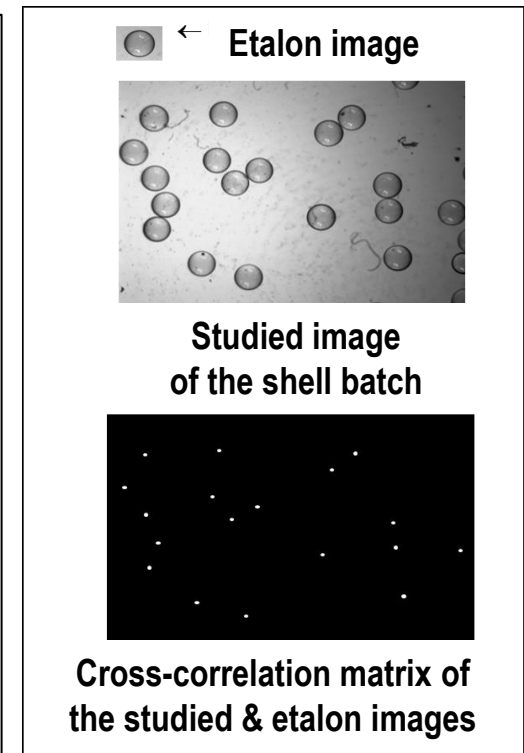
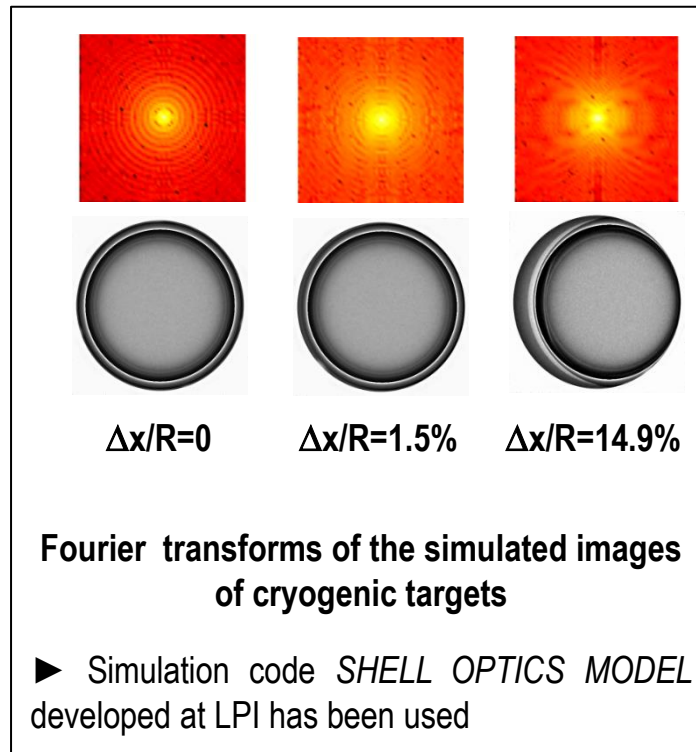
- Recognition of the target imperfections in both low- & high- harmonics
- Quality control of both a single target and a target batch
- Simultaneous control of the injected target quality, velocity & trajectory

Operation Principle:

Recognition signal is maximal if the real image is in strict conformity with etalon image

Operation Rate:

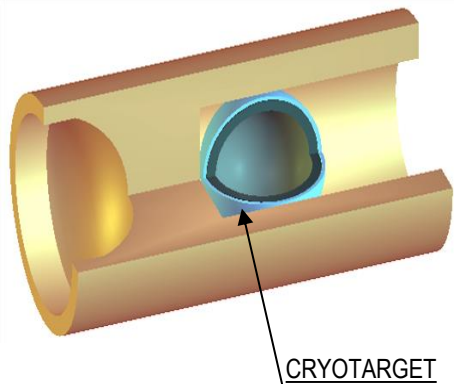
Operation rate of the Fourier holography scheme makes **several microseconds**



TARGET SURVIVAL RESUME \Rightarrow Successful target delivery requires both multiple target protective methods & ultra-fine fuel layers formation

PROTECTIVE SABOT

- we have optimized
- Shape of target support
 - Target injection temperature
 - Sabot material



Protective sabot with cryogenic target inside it

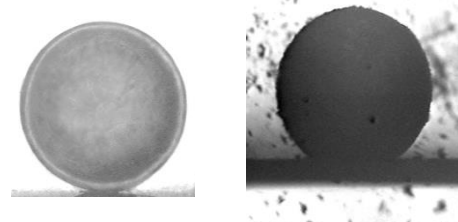
ISOTROPIC ULTRA-FINE FUEL LAYER with inherent survival features

- Withstand to higher heat- & g-loads than a crystalline layer
- No influence on shock wave propagation through isotropic ultra-fine fuel layer



Cryogenic target with the ultra-fine D_2 layer

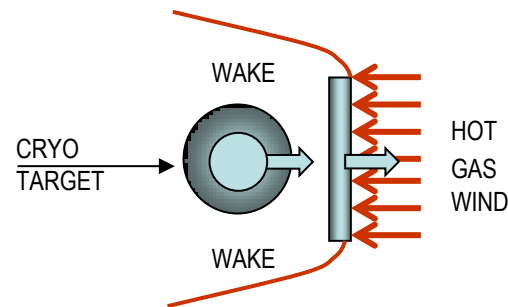
OUTER PROTECTIVE LAYERS



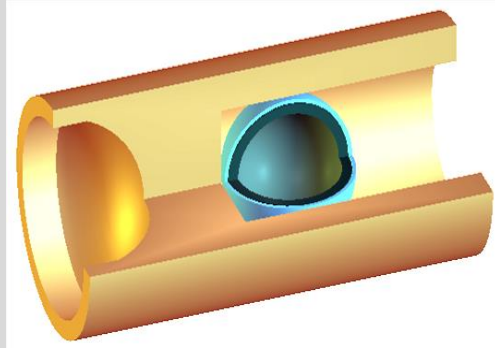
Cryogenic target with Pt/Pd outer layer (left) and with solid O_2 outer layer (right)

PROTECTIVE COVER

forms a wake area in the fill gas to avoid convective heating



SABOT is USED at a STAGE of TARGET TRANSPORT & INJECTION INTO a REACTOR CHAMBER

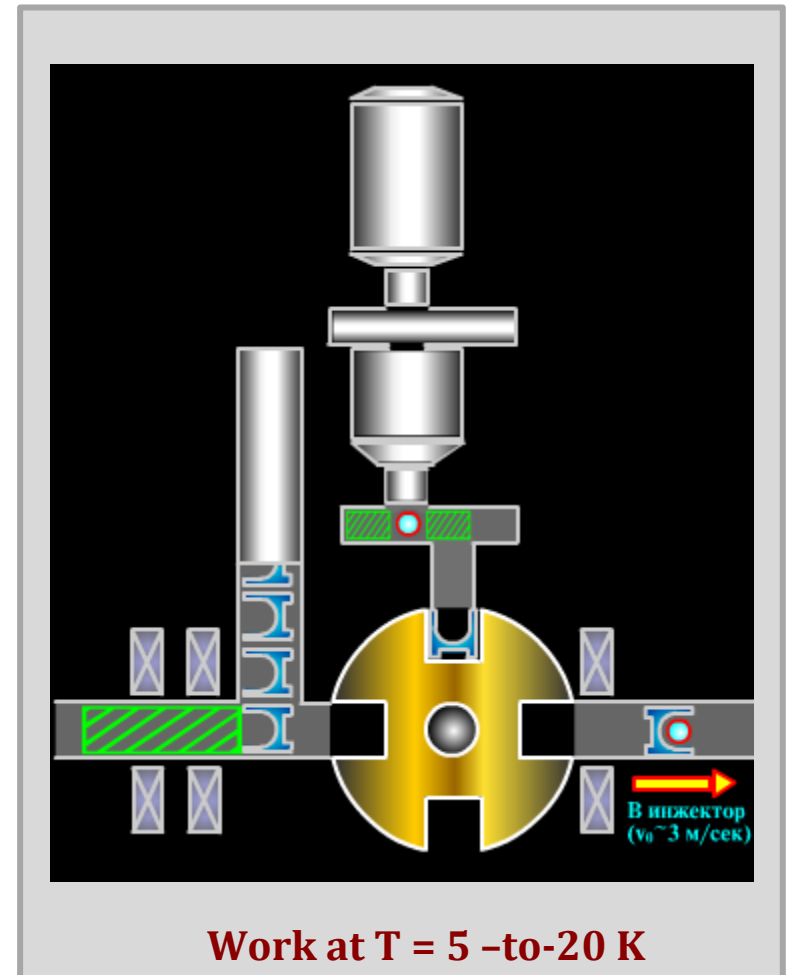


Target-&-Sabot assembly unit

■ SABOT is used for

- to transfer target from the LM to injector
- to transfer of an impulse of the movement on a target inside the injector
- to protect target from the heat- and g-loads arising during target acceleration

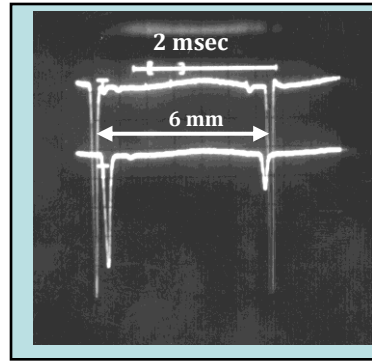
■ Concept of the device for Target-&-Sabot high rep-rate assembly



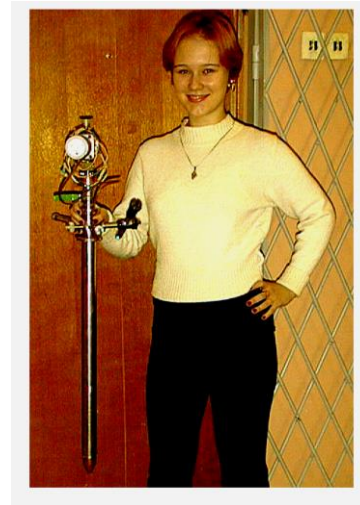
Prototyping a gravity assembly of "TARGET-&-SABOT" units at $T < 18K$ & refining a trajectory control of flying shells

Gravity injector (test setup)

developed by the LPI and the Rutherford
Appleton Laboratory (UK)
1989-1991

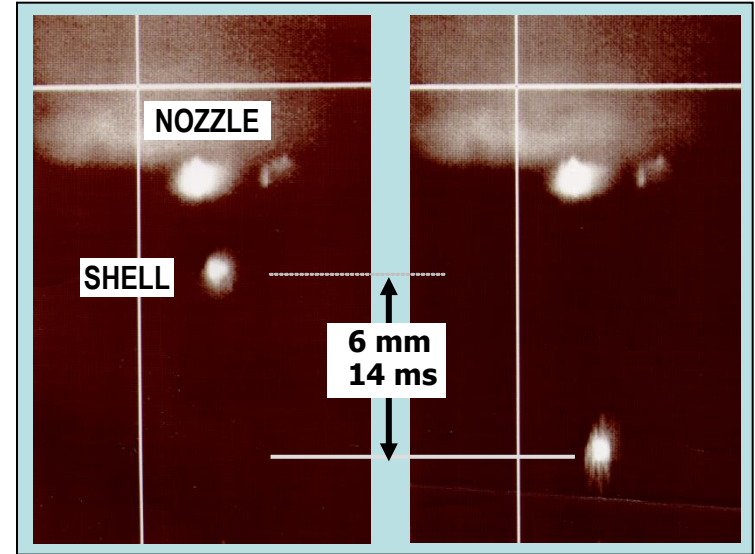


Double-beam oscilloscope
data of the injected shells



Prototype
of a gravity injector
integrated with
the FST-layering channel

High-speed video filming of injected shell into the test chamber; Video-camera *KODAK ECTAPRO 1000 IMAGER*



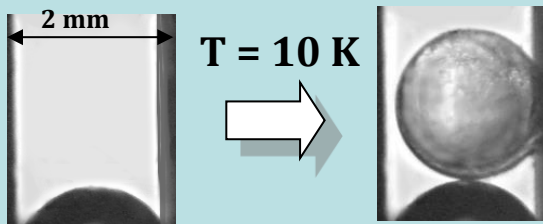
Refining *on-line* control of the flying shells trajectory

Data for 50 shots

(for CH shells of $\varnothing \sim 1$ mm)

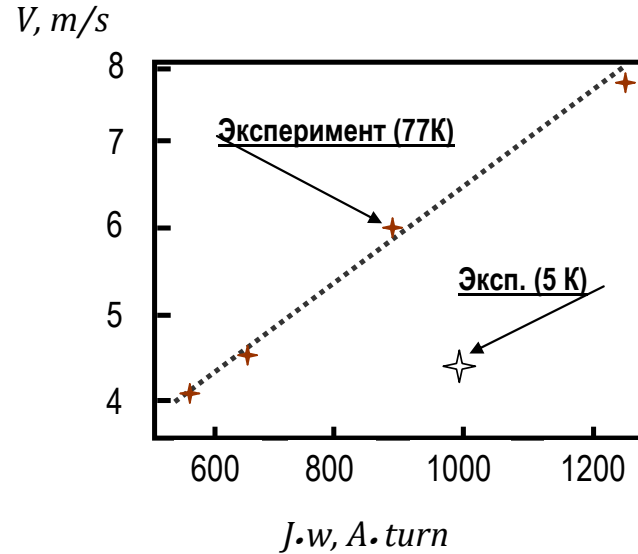
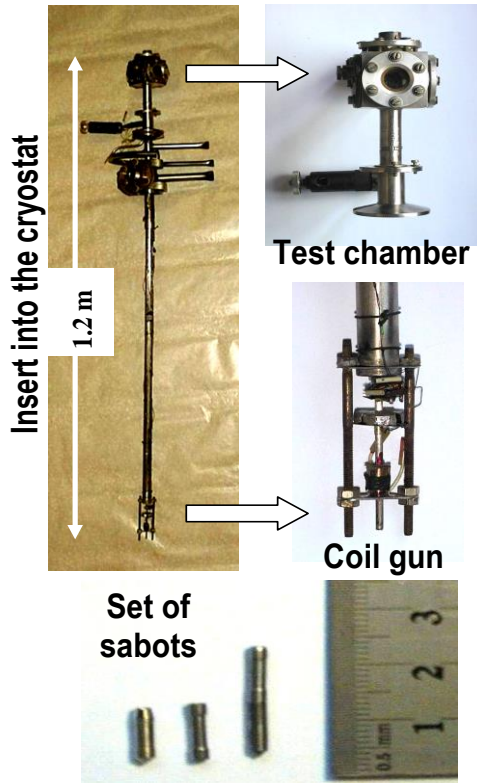
1. Trajectory angular spread ≤ 3 mrad
2. Injection velocity 0.43 - 0.55 m/s

Prototyping a gravity assembly of "Target-&-Sabot" at $T = 10$ K



Gravity delivery of cryogenic target
from the FST-layering channel
into a cylindrical cavity

Demonstration of the electromagnetic transport of sabot from soft ferromagnetic at cryogenic temperatures ($T = 77$ -to- 5 K)



Experiment: Sabot velocity

v (m/s) at the coil exit vs. $J\omega$

Maximal overloads:

$a = 320g$ (at $v = 8$ m/s)



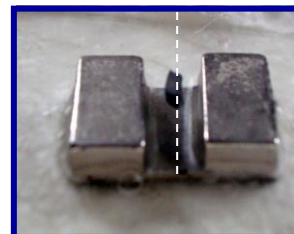
- ❑ **Experiment:** Magnetic penetration of ARMCO iron is enough high at cryogenic temperatures. This makes it possible to accelerate sabot up to 3 - 8 m/s using only one coil. These velocities ensure target transport at a start position in the injector.

❑ Problems:

1. Heat-loads due to sabot/guiding bore friction
2. Sabot tilting & wedging inside guiding bore

Resume: sabot trajectory correction & elimination of friction are needed

- ❑ **Correction of a trajectory of a cylindrical HTSC sabot using the magnetic field** (RFBR proj. #15-02-02497)



Experiment: HTSC sample (8x2x2 mm) aligns along the line of minimal magnetic induction between 2 rectangular permanent magnets, $T=80K$

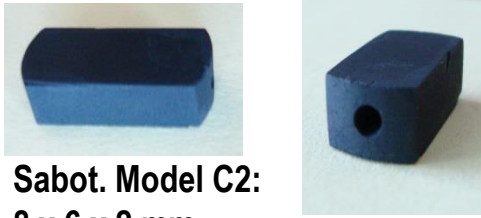
HTSC QUANTUM LEVITATION EFFECT FOR TARGET HANDLING & TRANSFER:

We have studied the HTSC samples made by different technology

I

YBa₂Cu₃O samples

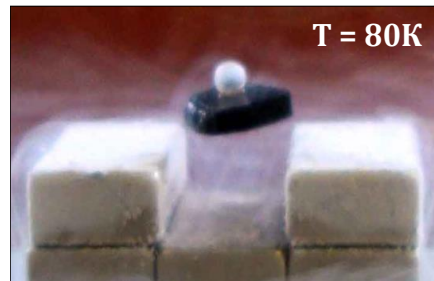
created by the technology of solid phase reactions (made at LPI)



Sabot. Model C2:
8 x 6 x 2 mm



Sabot. Model C3:
OD 5 mm, ID 2 mm, length 16 mm

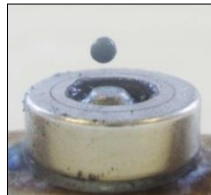
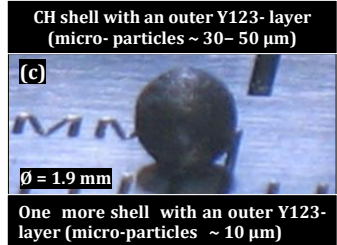
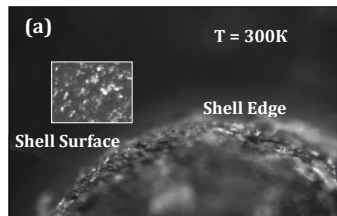


HTSC substrate (with CH shell on it) levitating over the PMG-1

II

HTSC coated CH shells.

HTSC layer: YBa₂Cu₃O powder distributed over the polymer matrix (made at LPI)



HTSC coated CH shell levitating over the PMG-2 at T = 80 K

III

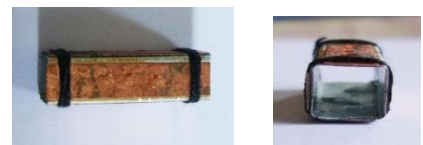
HTSC tape:

12 mm-width, 65-um total thickness including 1 um-thick epitaxial GaBa₂Cu₃O film

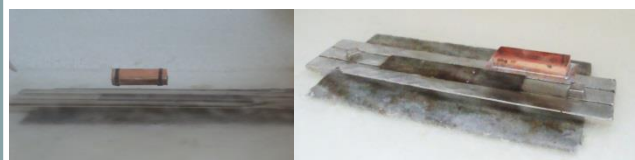
Technology: thin films deposition using laser ablation (made at SuperOx, Moscow)



Sabot. Model CX:
8 x 4 mm, length 24 mm



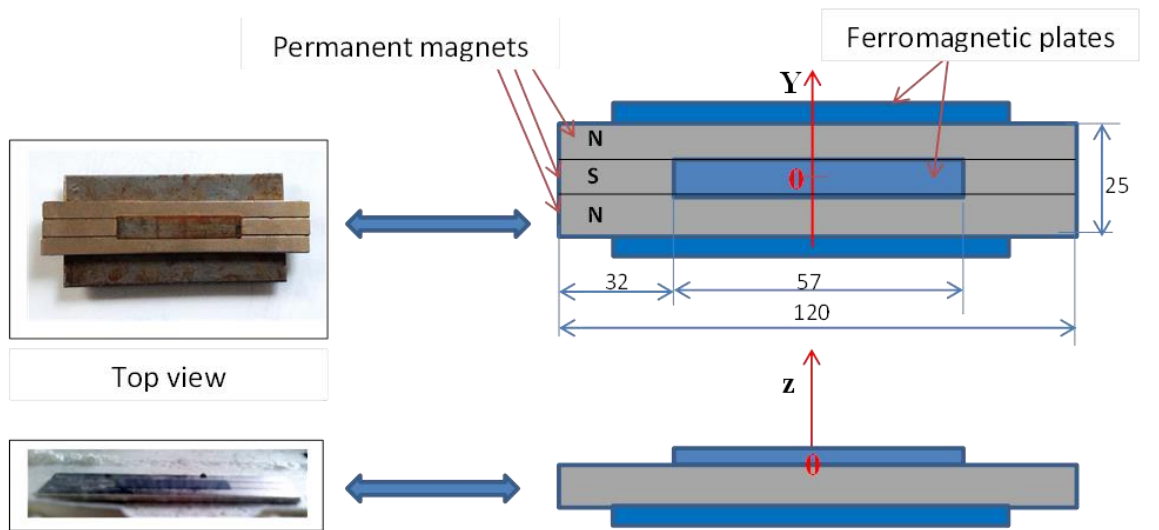
Sabot. Model C1:
5 x 5 mm, length 16 mm



Sabots C1 and CX levitating over the PMG-3 at T = 80 K

*/ PMG = permanent magnets guideway

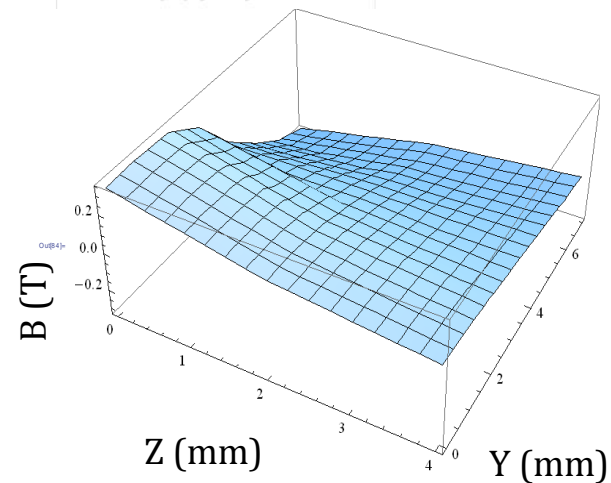
Permanent Magnetic Guideway (PMG-3): magnetic braking of lateral motion of the HTSC samples (demo at $T = 80\text{ K}$)



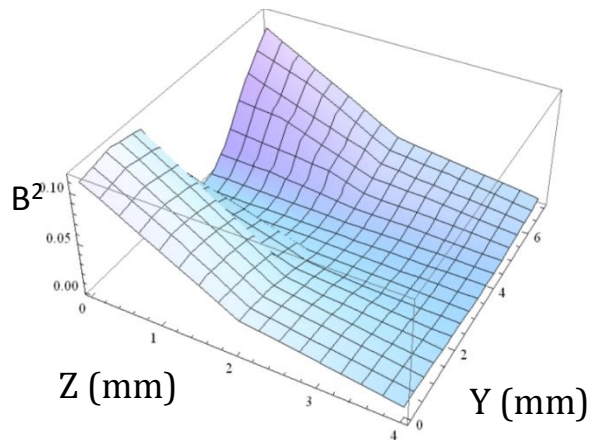
Top view



Side view



Field distribution



Distribution of B^2 : min is seen near the pole

- ❑ PMG-3 is a composition of NdFeB magnets & SFM tape
- ❑ HTSC samples made at LPI



$\text{YBa}_2\text{Cu}_3\text{O}$ coated CH shell of $\varnothing 2\text{ mm}$

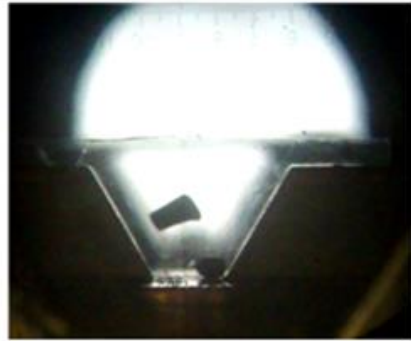


$\text{YBa}_2\text{Cu}_3\text{O}$ pellet of 12.4 mm-diam, 1-mm-thick

HTCS material study: HTSC samples stable levitation & movement in the magnetic field of the permanent magnets

- Stable levitation of HTSC samples at different temperatures (NdFeB magnets)

T = 6K -to- 18K,
HTSC sample from
 $\text{YBa}_2\text{Cu}_3\text{O}$ (made at LPI)
6x2x2 mm



T = 80 K,
HTSC sample from
 $\text{YBa}_2\text{Cu}_3\text{O}$ (made at LPI)
6x2x2 mm



- Ordered motion of HTSC carrier with CH shell over the magnetic rails (SrBa ferrite magnets)



T = 80 K, PMG-3a CH shell: \varnothing 2 mm (made at LPI)
HTSC carrier: $\sim 5 \text{ mm}^2$, $\text{YBa}_2\text{Cu}_3\text{O}$ (made at LPI)

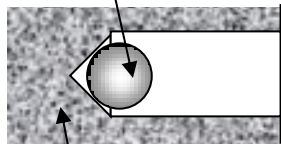
- HTSC sample cycling over the magnetic rails (NdFeB magnets)



T = 80 K, PMG-4
HTSC tape (SuperOx, Moscow):
12 mm-width, 65-um total thickness including
1 micron-thick **epitaxial $\text{GaBa}_2\text{Cu}_3\text{O}$ film**

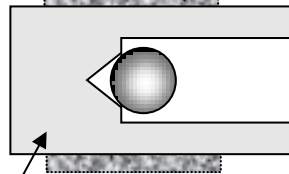
Conception of electromagnetic injector with HTSC sabot (HTSC material is under consideration)

1 Cryogenic target



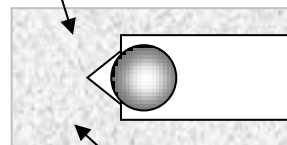
Sabot from bulk HTSC

2 HTSC outer layer



Magneto-dielectric (MD):
Fe-particles distributed over the polymer matrix

3 MD



Micro-particles from HTSC & Fe,
distributed over the polymer matrix

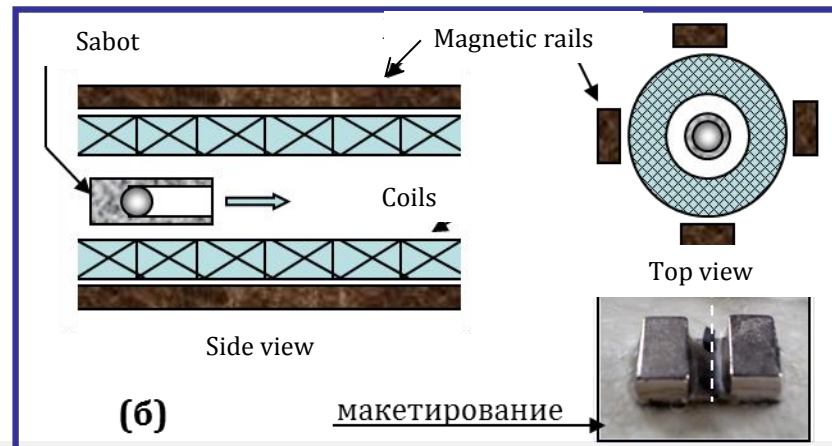
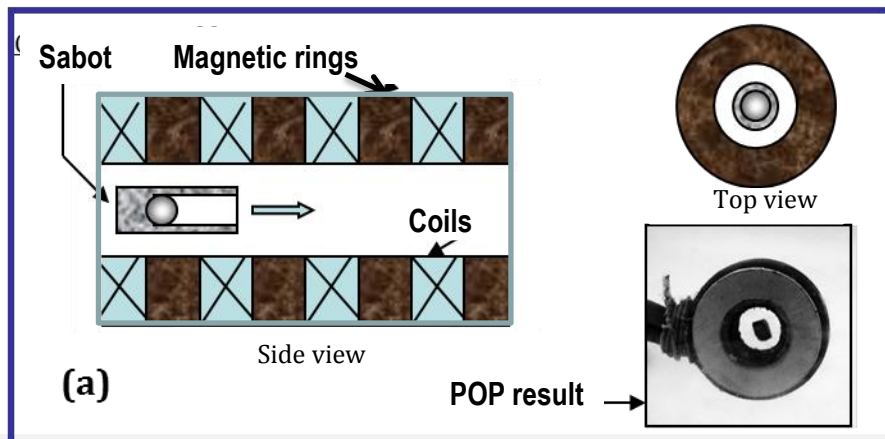


HTSC sabot acceleration
using one coil (movement
over the PMG-3).
Current: 200 A, 1 ms

Sabots for almost frictionless motion inside the electromagnetic injector, which enhance the operating efficiency of maglev accelerator



IMG_2453++.MOV



E-m injector + HTSC projectile. A design options with the HTSC sabot

Ref.: The possibility of HTSC sample acceleration using 2 coils has been proved in model experiments carried out in Gifu Univ., Japan [H.Yoshida, 3rd IAEA TM, Oct. 2004, Rep.Korea]

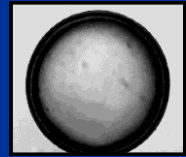
The next step is our new project started in December 2015 under IAEA contract # 20344/R0

- ❑ **Project title:** FST transmission line for mass manufacturing of IFE targets
- ❑ **Project goal** is modeling (exp. & theory) of the fabrication and injection processes of an FST transmission line for mass manufacturing of IFE targets.
- ❑ **Project approach** is the FST layering method developed at LPI.
- ❑ **Project targets** are CH shells of $\varnothing \sim 4$ mm, and the layer thickness of ~ 200 um for pure solid fuel and of ~ 300 um for in-porous solid fuel.
- ❑ **Our background for this project presented at**
 - 1st Meeting of IAEA CRP on Pathways to Energy from Inertial Fusion: Materials beyond Ignition (Feb. 2016, Vienna, Austria)
 - 7th IAEA TM on Physics and Technology of IFE Targets & Chambers (March 2015, Vienna, Austria)
 - 25th IAEA FEC (Oct. 2014, St. Petersburg, Russia)

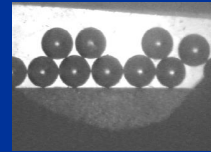


SUMMARY

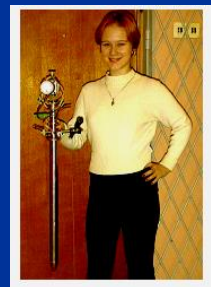
- ❑ FST layering method has been developed at LPI, which forms an isotropic ultrafine & spherical fuel layer inside unmounted free-rolling targets
- ❑ Our study has shown that application of such layers makes the risk of layer destruction minimal during cryogenic target delivery - **ISTC #1557, IAEA #13871**
- ❑ A full scaled scenario of the FST transmission line operation has been demonstrated at a small scale (targets $< \varnothing 2$ mm) - **ISTC #512, IAEA #11536**
 - ⇒ Fueling a batch of free-standing targets (up to 1000 atm D₂ at 300 K),
 - ⇒ Fuel layering using FST technology: cryogenic layer up to 100 μ m-thick,
 - ⇒ Target injection into the test chamber with a rate of 0.1 Hz
 - ⇒ Target tracking using the Fourier holography approach (computer expts)
- ❑ A number of injectors has been considered to study the cryogenic target delivery, including gravitation, electromagnetic and maglev one
- ❑ A number of POP experiments prove the efficiency of using the HTSC quantum levitation effect for free-standing target positioning & transport. **We continue the study in the frame of the RFBR project # 15-02-02497.**
- ❑ A prototypical FST layering module for rep-rate production of HiPER-scaled cryogenic targets has been designed based on the results of calculations and mockups testing. **Work was accomplished in the frame of EU project HiPER.**
- ❑ LPI continue developing the R&D program on CTF-LPI in the frame of new generation project under **IAEA contract # 20344/R0 (started at Dec. 2015)**



Cryo target with ultrafine fuel layer ($\varnothing 1.5$ mm)



Targets rep-rate injection under gravity: 0.1Hz, 5K



Cryogenic gravity injector



HTSC maglev for target positioning & transport